

TITLE OF THE INVENTION

METHOD OF MACHINING GLASS SUBSTRATE AND METHOD OF
FABRICATING HIGH-FREQUENCY CIRCUIT

5 BACKGROUND OF THE INVENTION

Field of the Invention

The present invention relates to a method and apparatus for fabricating a high-frequency circuit substrate of which smaller dielectric losses are desired.

10 In particular, the invention relates to a method of creating a circuit intended for higher frequency bands such as microwave bands and millimeter wave bands, and an apparatus using the same.

15 Description of Prior Art

It is desirable for substrates to be used in microwave, millimeter-wave, and other high-frequency circuits to be made of material having low-dielectric-loss properties so as to suppress dielectric losses in the
20 circuits resulting from the substrates themselves.

Fig. 1 is an explanatory diagram showing that the inherent dielectric loss of a substrate's own affects a signal flowing on a transmission line. Fig. 1 is a cross-sectional view of the circuit substrate as cut
25 perpendicular to the signal flowing on the transmission

line. The reference numeral 101 represents the substrate, 102 the transmission line, 103 a ground electrode, and 104 electric lines of force occurring when an electric signal flows on the transmission line 102. As shown in Fig. 1, the passage of an electric signal through the transmission line 102 makes the electric lines of force 104 run inside the substrate 101. Here, the electric lines of force 104 undergo the influence of the dielectric loss (given by the value of dielectric loss tangent) inherent to the substrate 101. A loss on the transmission line is given by:

$$\text{loss} = \text{factor} \times \text{frequency of circuit in question} \\ \times (\text{permittivity of substrate})^{1/2} \times \text{dielectric} \\ \text{loss of substrate (dielectric loss tangent)}.$$

The loss caused here converts into thermal energy, causing a phenomenon of heating the substrate.

Fabricating a high-frequency circuit involves the phenomenon described in Fig. 1. Therefore, a substrate having properties of lower permittivity and lower dielectric loss is selected for use. Substrates made of typical organic materials, at low frequencies, show the properties of lower permittivity and lower dielectric loss. In microwave and millimeter-wave bands of 1 GHz or higher, however, the substrates significantly deteriorate in permittivity due to the materials' potential polarization and frequency response, and thus are not often selected as

substrates for use in high frequencies (approximately 1 GHz or higher). For high frequencies, it is common to select inorganic materials such as alumina (permittivity: approximately 9, dielectric loss tangent: approximately 0.001), zirconia (permittivity: approximately 8, dielectric loss tangent: approximately 0.001), and aluminum nitride (permittivity: approximately 8, dielectric loss tangent: approximately 0.001).

Glass such as quartz is low in permittivity (permittivity: approximately 4) and in dielectric loss (dielectric loss tangent: 0.001 or lower) as compared to the inorganic materials. Therefore, it seems to be a promising material for high-frequency substrates for microwave and millimeter-wave bands. However, it is difficult to apply partial machining required of circuit substrates such as "through hole formation" to glass. Accordingly, it has been seldom used for high-frequency circuit substrates heretofore.

When glass is selected as the substrate material, ultrasonic machining appears to be the effective means for forming through holes in the glass substrate. The reason why chemical processing methods such as etching are not used for glass machining is that glass is a stable material. That is, although glass can be etched by solutions of hydrofluoric acids, phosphoric acids, alkalis, or the like,

etching rates are extremely low (nearly 1 $\mu\text{m}/\text{h}$ or so). As for sandblasting, sandblasting is capable of in-depth machining only twice or so the thickness of a mask. For example, in the case of forming 100- μm -diameter through
5 holes, the holes cannot be formed beyond 200 μm or so in depth, relative to the mask pattern having 100- μm openings. Here, no through hole can be made if the glass substrate is thicker than 200 μm .

When ultrasonic machining is used to machine a glass
10 substrate, a 100- μm hole in a 500- μm -thick substrate can be made at a machining rate of 1 sec or faster. Besides, the shape of the tool (horn) used in the ultrasonic machining can be devised to make a plurality of holes at a time. Nevertheless, the ultrasonic machining wears the tool in
15 operation, which requires a replacement with a new tool after several times of machining to glass substrates. In addition, there are limitations on the dimensions of the tools. Therefore, the ultrasonic machining is a method
20 hard to apply to mass production processes of large area glass substrates.

Meanwhile, laser beam machining has been already applied to mass production processes including the formation of through holes in alumina substrates and the like intended for high-frequency circuits, without any
25 limitations on substrate sizes. The laser beam machining

is, thus, suitable for ordinary substrate machining,
whereas its application to glass substrates gives rise to
the following problems. A YAG laser, a typical solid-state
laser, has a laser wavelength ($1.06\text{ }\mu\text{m}$) which is

5 transparent to glass. Therefore, the YAG laser is hard to
apply to glass machining. Concerning excimer laser
machining, the present inventors made machining experiments
on quartz glass of $500\text{ }\mu\text{m}$ in thickness by using a KrF
excimer laser (wavelength: $0.248\text{ }\mu\text{m}$), and obtained the
10 following results. That is, through holes of the order of
 $100\text{ }\mu\text{m}$ in diameter could be made at an energy density of
approximately 25 J/cm^2 . Nevertheless, the process
conditions had an extremely narrow range such that any
smaller energy densities preclude the machining while any
15 greater energy densities create large cracks in glass
substrates. This means that the excimer laser machining is
an inappropriate method for machining a glass substrate, in
terms of application to mass production processes.

It is conceivable that the use of an F_2 excimer laser
20 having a wavelength ($0.157\text{ }\mu\text{m}$) shorter than that of the KrF
excimer laser could somewhat relax the narrow range of the
process conditions for glass substrates. F_2 gas is,
however, poisonous to humans and therefore the use of the
 F_2 excimer laser in mass production processes is
25 unrealistic.

Now, turning to the case of machining a glass substrate by using an ultrashort-pulse laser so-called femtosecond laser which has a pulse width of no greater than 10^{-13} seconds. As described in e.g. "Interaction
5 Between Light and Glass by Ultrashort Pulse Laser -Growing Frequency Conversion Crystal in Glass-" (pp.67-73), *MATERIALS INTEGRATION* vol. 13, no. 3 (2000), the machining to the glass substrate is possible. However, due to high prices and high running costs of ultrashort-pulse laser
10 systems, the application to mass production processes is difficult.

A machining method using a CO₂ laser that is used for forming through holes and the like in an alumina substrate can be adopted to execute the perforation of glass
15 substrates under process conditions wider than for the excimer lasers. In addition, since CO₂ laser systems are lower in price and in running costs than the other systems, it can be said that the CO₂ laser machining is a glass substrate machining method suited to mass production.

20 Nevertheless, machining glass substrates by using the CO₂ laser produces the problem to be described below.

Fig. 2 is a diagram showing the problem that arises when a glass substrate is machined by using a CO₂ laser of variable pulse width. In Fig. 2, the reference numeral 201
25 represents the glass substrate, and 202 a through hole

formed by the laser. Moreover, 203 represents upheaval
that occurs upon the formation of the through hole 202, 204
the hole diameter of the glass substrate 201 on the laser-
irradiated side (top hole diameter), and 205 the diameter
5 on the side opposite to the laser-irradiated side (bottom
hole diameter). As shown in Fig. 2, the through hole 202,
being formed in the glass substrate 201 by using the CO₂
laser of variable pulse width, has a tapered shape as seen
in Fig.2 with the upheaval 203 on the top rim. The ratio
10 of the bottom hole diameter 205 to the top hole diameter
204 and the amount of the upheaval 203 can be modified by
changing the pulse width of the laser to adjust the pulse
energy applied to the glass substrate. It is impossible,
however, to avoid the tapered shape and the upheaval
15 phenomenon.

SUMMARY OF THE INVENTION

The present invention has been achieved in view of
the conventional problems described above. It is thus a
20 first object of the present invention to provide a laser-
based glass substrate machining method capable of coping
with mass production processes.

A second object of the present invention is to use
this glass substrate machining method to make a low-
25 permittivity, low-dielectric-loss glass substrate

applicable as the substrate of a high-frequency circuit intended for microwave and millimeter-wave bands in particular.

5 A third object of the present invention is to use the above-mentioned substrate achieved by the glass substrate machining method to enhance performances of a radio terminal apparatus and the like.

10 The present invention is to achieve the foregoing objects through contrivances both to the glass substrate itself and to the laser beam machining method. Specifically, a glass substrate is provided in which the amount of air bubbles in glass is appropriately controlled to improve the workability of the substrate itself. Then, the glass substrate is irradiated with a pulsed laser over 15 a plurality of times during machining, thereby improving the machining shape to the glass substrate.

To realize the technique as described above, the present invention features that the amount of air bubbles in the glass substrate is controlled to improve the laser 20 workability of the glass substrate itself.

Moreover, the present invention provides a glass substrate machining method for machining a glass substrate by using a laser, comprising the step of controlling the amount of air bubbles in the glass substrate to improve the 25 workability of the glass substrate, in which a thin

insulator is formed on the glass surface. In this case, the thin insulator on the glass surface may be glass formed by coating. Alternatively, the insulator may be an organic insulator film. When the insulator is an organic insulator
5 film, the thin organic insulator on the glass surface may be formed by coating. Furthermore, the thin insulator formed on the glass surface may be made into a sheet form by using a laminator.

In addition, the present invention provides a method
10 for machining a glass substrate by using a laser, comprising the step of controlling the amount of air bubbles in the glass substrate to form a vacancy only inside of the glass substrate.

Moreover, the present invention provides a method of
15 forming a metal film on a glass substrate, wherein the amount of air bubbles in a glass substrate is controlled so that the glass substrate, after laser machining, has a large surface area on the machined surface due to bubble traces in glass, thereby performing electroless plating
20 simply.

The present invention is also characterized in that:
the amount of air bubbles in a glass substrate is controlled so that the glass substrate, after laser machining, has a large surface area on the machined surface
25 due to bubble traces in glass; and a metal film is formed

to improve heat radiation property of the metal-film-formed portion.

The present invention is also characterized in that a CO₂ laser is used for laser machining.

5 Furthermore, the present invention provides a glass substrate machining method for using a CO₂ laser of variable pulse width as machining means, the method comprising: a first step of executing a single laser irradiation; and a second step of executing a plurality of
10 laser irradiations.

The present invention also provides the glass substrate machining method described above, wherein the pulse width of the laser in the second step is greater than that in the first step.

15 Furthermore, the present invention provides a method of fabricating a high-frequency circuit by using the glass substrate machining method having the characteristics described above.

Moreover, the present invention provides a radio
20 terminal apparatus comprising a high-frequency circuit fabricated by using the glass substrate machining method having the characteristics described above.

The present invention also provides a radio base station apparatus comprising a high-frequency circuit
25 fabricated by using the glass substrate machining method

having the characteristics described above.

The present invention also provides a radar apparatus comprising a high-frequency circuit fabricated by using the glass substrate machining method having the characteristics described above.

As has been described, according to the present invention, glass substrates which are typically difficult to machine can be easily applied to the fabrication of high-frequency circuits. This allows wide, public supply of high-performance circuits and apparatuses.

The foregoing objects and advantages of the present invention will become more apparent from the following description when read in conjunction with the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a conceptual diagram showing a problem that occurs when a conventional glass substrate is used;

Fig. 2 is a conceptual diagram showing a problem that occurs when laser machining is applied to a conventional glass substrate;

Figs. 3(a) and 3(b) are explanatory diagrams showing a method of machining a glass substrate according to an embodiment of the present invention;

Figs. 4(a) and 4(b) are explanatory diagrams showing

how a glass substrate is machined with a laser;

Fig. 5 is an explanatory diagram showing a method of machining a glass substrate according to an embodiment of the present invention;

5 Fig. 6 is an explanatory diagram showing a method of machining a glass substrate according to an embodiment of the present invention;

10 Fig. 7 is an explanatory diagram showing a method of machining a glass substrate according to an embodiment of the present invention;

Fig. 8 is an explanatory diagram showing a method of machining a glass substrate according to an embodiment of the present invention; and

15 Figs. 9(a) and 9(b) are explanatory diagrams showing a method of machining a glass substrate according to an embodiment of the present invention.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

Hereinafter, an embodiment of the present invention
20 will be described with reference to the drawings. Figs. 3(a) and 3(b) are cross-sectional views of a substrate consisting of glass that bears air bubbles. Fig. 3(a) shows a state before laser beam machining, and Fig. 3(b) a state after laser beam machining. In Figs. 3(a) and 3(b),
25 the reference numeral 1 represents the glass substrate, 2

bubbles in the glass substrate, and 3 a through hole formed by laser beam machining.

The method for fabricating the bubble-bearing glass shown in Fig. 3(a) is publicly known as described in e.g.

5 Japanese Patent Laid-Open Publication No.Hei 10-29836.

Glass substrates with designated amounts of bubbles are made available by requesting from substrate suppliers.

When a glass substrate bearing such a controlled amount of bubbles is used as a substrate intended for high-frequency
10 circuits, it offers even the effect of reducing a loss

during signal transmission since the substrate having a permittivity yet lower than those of ordinary glass

substrates is in use. When the substrate consisting of bubble-bearing glass as shown in Fig. 3(a) is perforated by
15 using a laser beam, the ratio of the hole diameter on the

laser-irradiated side (top hole diameter) to the hole diameter on the side opposite to the laser-irradiated side (bottom hole diameter) approaches 1 as shown in Fig. 3(b).

The upheaval 203 shown in Fig. 2 is also suppressed

20 significantly. The reason for this is that while the laser irradiation thermally machines the glass, minute cracks successively arise between minute bubbles in the glass along the direction of the laser irradiation. These cracks propagate consecutively from the laser-irradiated side to
25 the side opposite to the laser-irradiated side, thereby

causing a machining phenomenon. As a result, machining with a smaller tendency to taper is achieved.

Moreover, the laser pulse energy necessary for forming the through hole in this glass substrate can be made several tens of percentages or much lower than that in forming a through hole in ordinary glass substrates. This can suppress the production of the upheaval shown in Fig. 2. Furthermore, the bubbles in the glass function to inhibit the heat inside the glass produced by the laser irradiation from diffusing in lateral directions of the glass substrate. This means that the laser-based thermal machining is performed effectively in the direction of the laser irradiation. Incidentally, due to the thermal machining by the laser beam, the laser-machined through hole has a smooth surface with asperities resulting from bubble traces that have molten away. Concerning the types of lasers to be used here, a CO₂ laser is more advantageously used for mass production processes. Nevertheless, KrF and other excimer lasers can also be used in the perforation to involve the crack-propagating machining of the bubbles. Here, the narrow process conditions for ordinary glass substrate machining are relaxed, and the glass machining itself can be performed satisfactorily under energy lower than in the ordinary glass substrate machining.

Among techniques for further improving the machined

shape of the through hole 3 shown in Fig. 3(b) is a machining method using a CO₂ laser of variable pulse width, comprising a first step of performing laser irradiation only once and a second step of performing laser irradiation over a plurality of times. This method allows both the suppression of the taper and the suppression of the upheaval of the machined portion even in ordinary glass machining. Figs. 4(a) and 4(b) show how a glass substrate is perforated by using the CO₂ laser of variable pulse width which can suppress the taper and the upheaval of the machined portion even in ordinary glass machining. Figs. 4(a) and 4(b) both are cross-sectional views of a glass substrate 201 in which a through hole 202 is formed. Fig. 4(a) shows a cross section of the glass substrate having undergone only a single laser irradiation at the first step. Fig. 4(b) shows a cross section of the glass substrate having undergone a plurality of laser irradiations at the second step. The reason why such a shape as shown in Fig. 4(b) is obtained through the execution of a plurality of laser irradiations on the glass substrate at the second step is that the plurality of laser irradiations can increase the hole diameter on the side opposite to the laser-irradiated side (bottom hole diameter). Here, the diameter of the laser beam is unchanged irrespective of the number of irradiations; therefore, the hole diameter on the

laser-irradiated side (top hole diameter) remains unchanged.

The reason why the execution of a plurality of laser irradiations at the second step reduces the upheaval is that an annealing effect on the periphery of the through hole evens out the upheaval. Applications of this machining method include a method of changing the pulse width of the laser irradiation between the first step and the second step, or shifting the focus of the laser in the depth direction of the through hole upon the second laser irradiation. These methods can be combined to form a more perpendicular through hole in a glass substrate. In this connection, the method of making the laser pulse width in the second step greater than in the first step, if adopted, enhances the annealing effect of suppressing the upheaval. When these methods are used to conduct the formation of a through hole in the substrate consisting of bubble-bearing glass shown in Fig. 3(a), a through hole of favorable shape can be formed with energy less than in ordinary glass machining. The machining method described above can be used to form not only the through holes but also grooves and vacancies which are difficult to form by ordinary glass machining.

Fig. 5 shows an example of the result of groove machining. In Fig. 5, the reference numeral 4 represents a groove formed in a section of a substrate 1 that consists

of bubble-bearing glass. This groove can be formed by shifting a laser beam relative to the bubble-bearing glass substrate. Fig. 6 shows a machining method for forming a vacancy inside a bubble-bearing glass substrate. In Fig. 6, the reference numeral 1 represents a substrate consisting of bubble-bearing glass, 5 a vacancy formed inside the glass, 6 a lens for focusing a laser beam, and 7 the laser beam. The laser beam 7 is condensed by the lens 6 into focus on a portion of 5 in the bubble-bearing glass substrate 1. In this condition, the laser beam and the substrate 1 are relatively shifted so that minute cracks successively occur between minute bubbles inside the glass substrate 1, along with thermal machining. This makes it possible to form the vacancy 5 inside the glass substrate 1.

In this connection, it is desirable to use here a laser having a higher peak output. Lasers of lower peak outputs, if used, fail to form vacancies, but the groove shape shown in Fig. 5 would result.

The machining methods described in conjunction with Figs. 3 and 5, when combined with an increase in the diameter of each bubble mixed in the glass substrate 1, can provide other effects. Here, in general the bubble diameter is desirably greater than or equal to 50 μm . Fig. 7 shows in cross section a glass substrate 1 bearing bubbles 2 of somewhat greater diameters, with a through

hole formed therein by a laser. In this glass substrate machining method, the wall of the through hole 3 undergoing the thermal effect of the laser becomes an uneven surface, not a completely smooth one, because the bubbles 2 are of a certain size. The uneven surface condition of the through hole acts to the advantage of circuit substrate fabrication. In typical circuit substrate fabrication, through holes are formed for the purpose of establishing electric connection between the circuits on the front and on the back. Metal films are formed over the walls of the through holes. For example, the metal films for electric connection are formed by electroless-plating thin metal films, and then electroplating the metal films up to a certain thickness (approximately 10 μm or smaller). This electroless plating step involves roughening, or a step of intentionally coarsening surfaces to be plated, because sufficient bond strength cannot be obtained if the surfaces are smooth. The provision of uneven through hole surfaces as in the present invention eliminates the need for the roughening step, and thus is advantageous for mass production and fabrication of circuit substrates.

Fig. 8 shows an example where a number of grooves are laser-formed in a glass substrate 1 bearing bubbles 2 of somewhat greater diameters. This kind of machining can create a surface having a surface area far greater than in

ordinary glass substrates. Such an uneven surface, if a metal film or other thin film of high heat conductivity is formed thereon, can make a surface of high heat radiation. Then, this surface can be applied to heat-radiation-

5 critical circuit substrates to fabricate high-performance circuit substrates.

In fabricating high-frequency circuits on bubble-bearing glass substrates, and particularly in the cases of adopting larger bubbles described in conjunction with Figs. 7 and 8, the surface roughness of portions for transmission lines to be formed on sometimes becomes crucial to the circuits which deal with high frequencies of a microwave band or a millimeter wave band. The reason is that the transmission lines formed on rough-surfaced substrates come to have asperities, which can cause losses in signal transmission and/or increase the actual line lengths because of increased surface areas. This problem can be avoided by forming insulator films on the surfaces of the bubble-bearing glass substrates. Figs. 9(a) and 9(b) show a method for solving the above-mentioned problem by forming an insulator on a bubble-bearing substrate 1.

Fig. 9(a) is a cross-sectional view of the substrate before laser beam machining, in which the reference numeral 8 represents an insulator. Concerning the material of the insulator 8, it is preferable to select a material having

planarization effect to asperities from among spin-on-glass (SOG) and other insulators which can be easily formed by coating. Moreover, polyimide, benzocyclobutene, and other organic insulator films can be formed with greater

5 thicknesses and improved asperity planarization effect as compared with SOG and other inorganic substances. The formation of the polyimide and benzocyclobutene films are typically formed by spin coating and a following step of hardening, through, but not limited to, coating-based
10 methods such as the spin coating. The organic films may be formed in a laminator. Fig. 9(b) shows a state where a through hole is formed by a laser. There lies an SOG or other inorganic material film of several micrometers, a polyimide or benzocyclobutene coating of the order of 10-50
15 μm , or a laminator-formed organic film of the order of 20-70 μm . These substances will not hinder the formation of the through hole 3 since they have far superior laser workability as compared to glass substrates. Forming transmission lines on the insulator 8 solves the above-
20 mentioned problem.

When high-frequency circuits are fabricated by using the method of machining a glass substrate according to the present invention, it becomes possible to manufacture circuits of higher performance and excellent mass
25 productivity. In addition, the high-frequency circuit

according to the present invention is applicable to radio portable terminals, radio base stations, radar apparatuses, and the like, and it is possible to produce high-performance mass-producible apparatuses.